

Page 17, line 12, and continuing onto page 18, line 1, has been amended as follows:

be The lead angle  $\theta$ , the groove depth H and the groove number N of the grooves 3 formed in the V-shaped patterns, the first to fifth groups A - E of which are arranged in the inner surface of the pipe, are set to the values by which the smallest flow resistance is obtained. In addition, the secondary grooves 6 are formed in the projected portions 5 provided between the respective grooves 3 as main grooves in V-shaped patterns and the secondary grooves 6 are notched grooves from the top 5a towards the base 5b of the projected portions 5 and are directed in the spiral direction. Therefore, since the flow resistance can be made as small as possible to reduce the pressure loss and swirling force in the spiral direction can be further increased, a heat-transfer pipe for a heat exchanger having a still higher performance can be obtained.--

Page 21, lines 9-24 have been amended as follows:

be The lead angle  $\theta$ , the groove depth H and the groove number N of the grooves 3 formed in the V-shaped patterns, the first to fifth groups A - E of which are arranged in the inner surface of the pipe, are set to the values by which the smallest flow resistance is obtained. In addition, the secondary grooves 7 composed of fine grooves are formed from one side of an outer surface of the projected portion 5 to the other side thereof to direct toward, for example, the spiral direction. Therefore, since the flow resistance can be made as small as possible to reduce the pressure loss and swirling force in the spiral direction can be further increased, a heat-transfer pipe for a heat exchanger having a still higher performance can be obtained. Also, even when the pipe is expanded, the fine grooves on the side portions are not crushed and thereby the heat transfer performance is not deteriorated.--